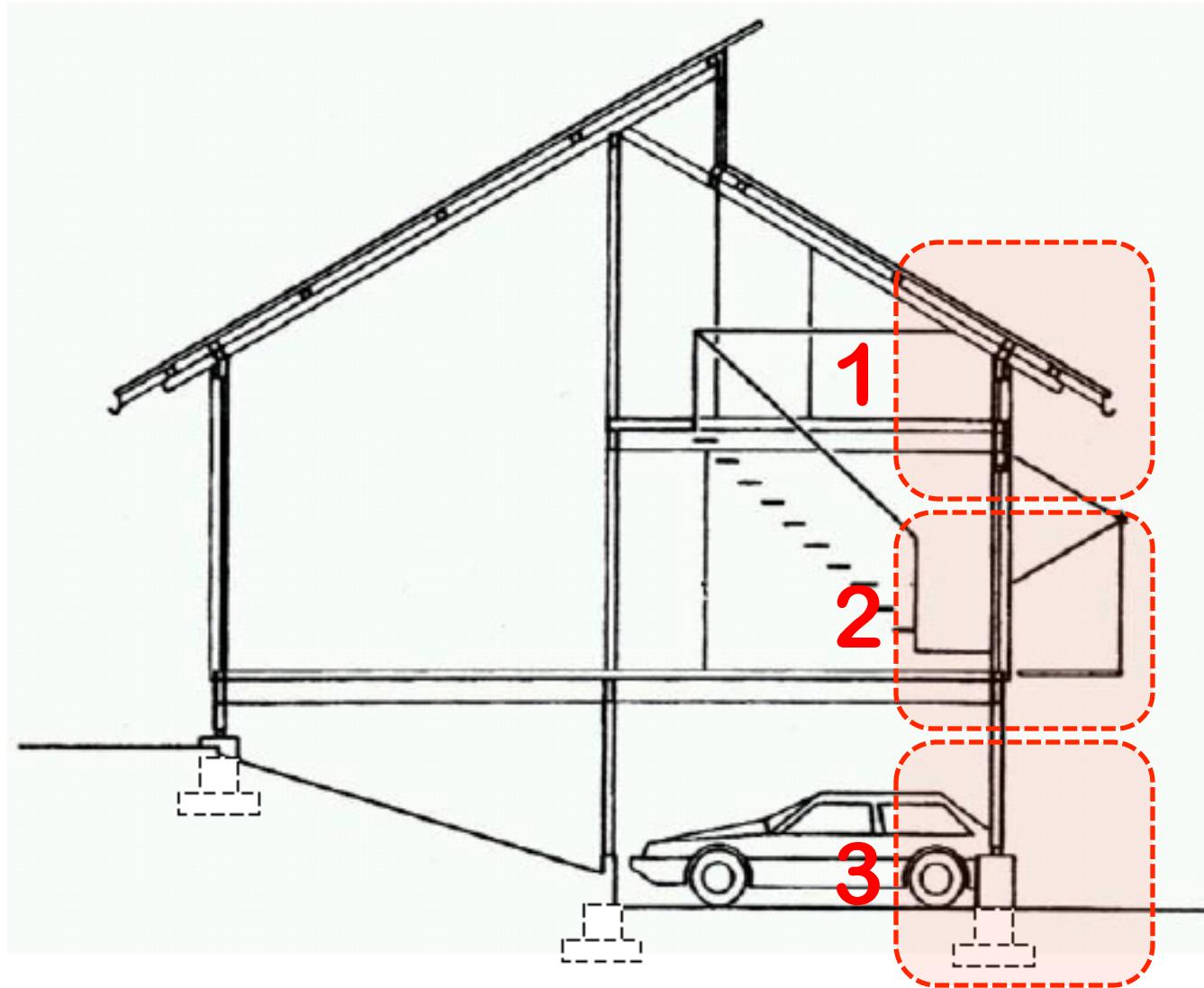


PERENCANAAN TEKNOLOGI & SISTEM BANGUNAN

(PTSB) 03



<i>Walls</i>	<i>lb/ft²</i>	<i>Masonry</i>	<i>lb/ft³</i>
Clay brick			
High-absorption, per 4-in wythe	34	Cast-stone masonry	144
Medium-absorption, per 4-in wythe	39	Concrete, stone aggregate, reinforced	150
Low-absorption, per 4-in wythe	46	Ashlar:	
Sand-lime brick, per 4-in wythe	38	Granite	165
Concrete brick		Limestone, crystalline	165
4-in, with heavy aggregate	46	Limestone, oölitic	135
4-in, with light aggregate	33	Marble	173
Concrete block, hollow		Sandstone	144
8-in, with heavy aggregate	55	<i>Roof and Wall Coverings</i>	<i>lb/ft²</i>
8-in, with light aggregate	35	Clay tile shingles	9 to 14
12-in, with heavy aggregate	85	Asphalt shingles	2
12-in, with light aggregate	55	Composition:	
Clay tile, loadbearing		3-ply ready roofing	1
4-in	24	4-ply felt and gravel	5.5
8-in	42	5-ply felt and gravel	6
12-in	58	Copper or tin	1
Clay tile, nonloadbearing		Cornigated steel	2
2-in	11	Sheathing (gypsum), ½-in	2
4-in	18	Sheathing (wood), per in thickness	3
8-in	34	Slate, ¼-in	10
Furring tile		Wood shingles	2
1½-in	8	<i>Waterproofing</i>	<i>lb/ft²</i>
2-in	10	Five-ply membrane	5
Glass block, 4-in	18	<i>Ceilings</i>	<i>lb/ft²</i>
Gypsum block, hollow		Plaster (on tile or concrete)	5
2-in	9.5	Suspended metal lath and gypsum plaster	10
4-in	12.5	Suspended metal lath and cement plaster	15
6-in	18.5	Suspended steel channel supports	2
		Gypsumboard per ¼-in thickness	1.1

<i>Floor Finishes</i>	lb/ft ²
Asphalt block, 2-in	24
Cement, 1-in	12
Ceramic or quarry tile, 1-in	12
Hardwood flooring, $\frac{7}{8}$ -in	4
Plywood subflooring, $\frac{1}{2}$ -in	1.5
Resilient flooring, such as asphalt tile and linoleum	2
Slate, 1-in	15
Softwood subflooring, per in of thickness	3
Terrazzo, 1-in	13
Wood block, 3-in	4

Wood joists, double wood floor, joist size	lb/ft ²	
	12-in spacing	16-in spacing
2 × 6	6	5
2 × 8	6	6
2 × 10	7	6
2 × 12	8	7
3 × 6	7	6
3 × 8	8	7
3 × 10	9	8
3 × 12	11	9
3 × 14	12	10

<i>Concrete Slabs</i>	lb/ft ²
Stone aggregate, reinforced, per in of thickness	12.5
Slag, reinforced, per in of thickness	11.5
Lightweight aggregate, reinforced, per in of thickness	6 to 10

<i>Floor Fill</i>	lb/ft ²
Cinders, no cement, per in of thickness	5
Cinders, with cement, per in of thickness	9
Sand, per in of thickness	8
<i>Partitions</i>	lb/ft ²
Plaster on masonry	
Gypsum, with sand, per in of thickness	8.5
Gypsum, with lightweight aggregate, per in	4
Cement, with sand, per in of thickness	10
Cement, with lightweight aggregate, per in	5
Plaster, 2-in solid	20
Metal studs	
Plastered two sides	18
Gypsumboard each side	6
Wood studs, 2 × 4-in	
Unplastered	3
Plastered one side	11
Plastered two sides	19
Gypsumboard each side	7
<i>Glass</i>	lb/ft ²
Single-strength	1.2
Double-strength	1.6
Plate, $\frac{1}{8}$ -in	1.6
<i>Insulation</i>	lb/ft ²
Cork, per in of thickness	1.0
Foamed glass, per in of thickness	0.8
Glass-fiber bats, per in of thickness	0.06
Polystyrene, per in of thickness	0.2
Urethane	0.17
Vermiculite, loose fill, per in of thickness	0.5

1 ft = 0,3048 m
1 in = 25,40 mm

1 lb/ft² = 16,019 kg/m²

lb = pounds

$$\sigma = \frac{F (k N)}{A (m^2)}$$

$$A = \frac{F (k N)}{\sigma (k N/m^2)}$$

The 2:1 method

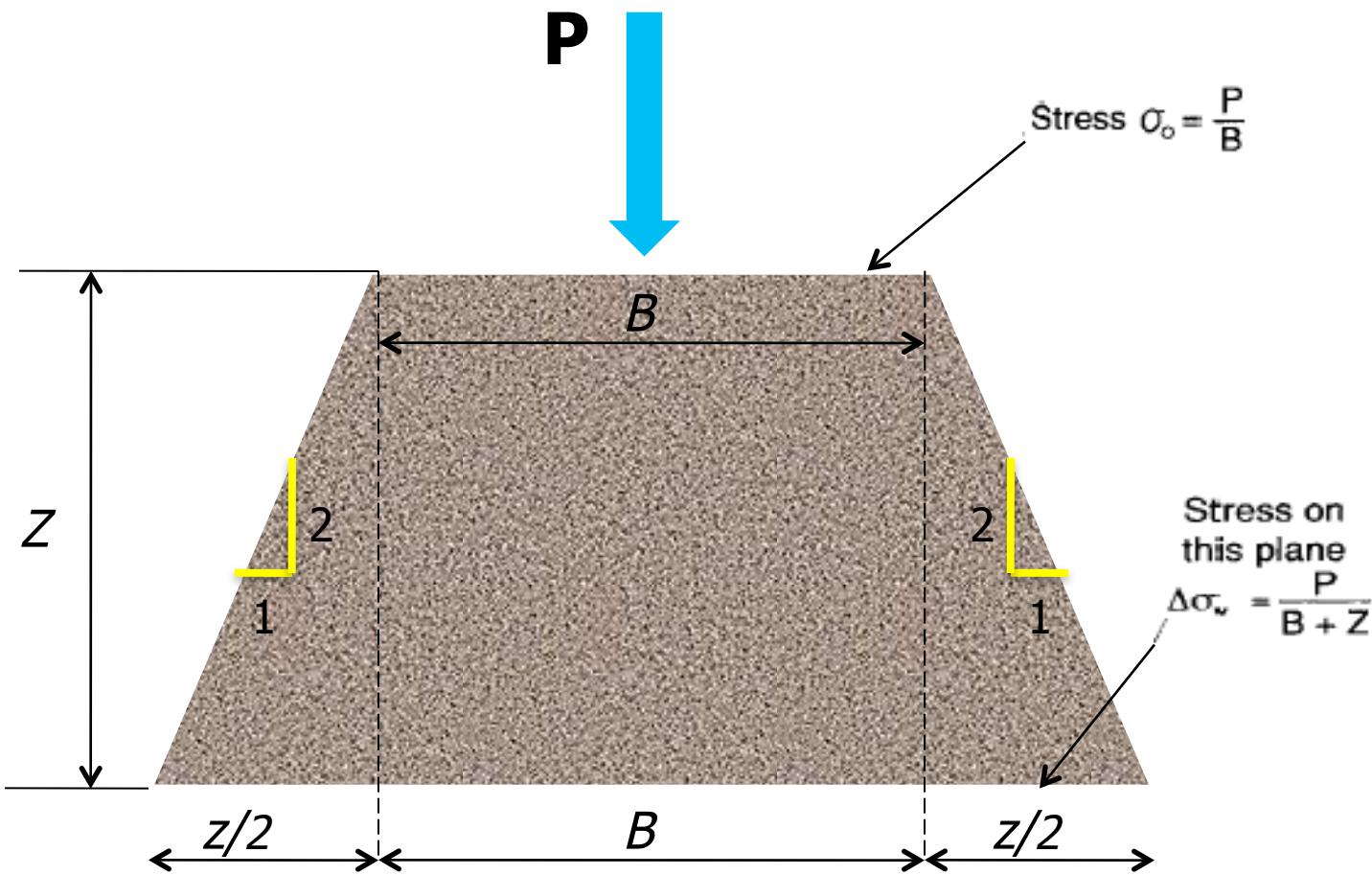
assumes that the stress dissipates with depth in the form of a trapezoid that has 2:1 (vertical: horizontal) inclined sides.

The purpose of this method is to approximate the actual ‘‘pressure bulb’’ stress increase beneath a footing.

$$\sigma_z = \Delta\sigma_v = \frac{P}{B + z}$$

If the footing is a rectangular spread footing having a length L and a width B, then the stress applied by the rectangular footing (σ_o) would be $\sigma_o = P / (BL)$ where P entire load of the rectangular spread footing.

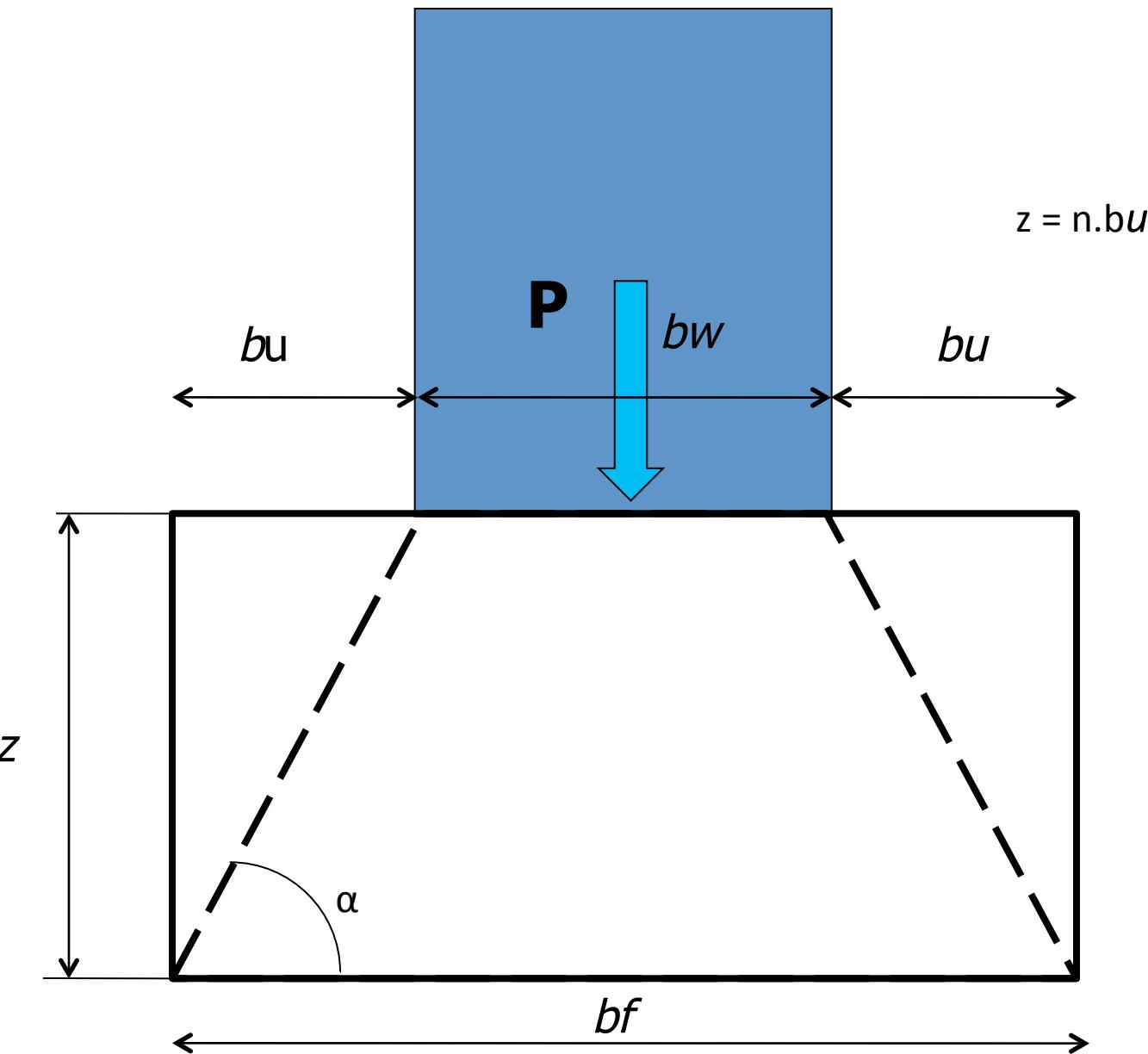
$$\sigma_z = \Delta\sigma_v = \frac{P}{(B+z)(L+z)}$$



If there is known $P = 200 \text{ kN/m}$, the wall thickness = 0.49 m, $\sigma = 240 \text{ kN/m}^2$, rectangular foundation length (l) = 1.00 m

using concrete B 15 determine:

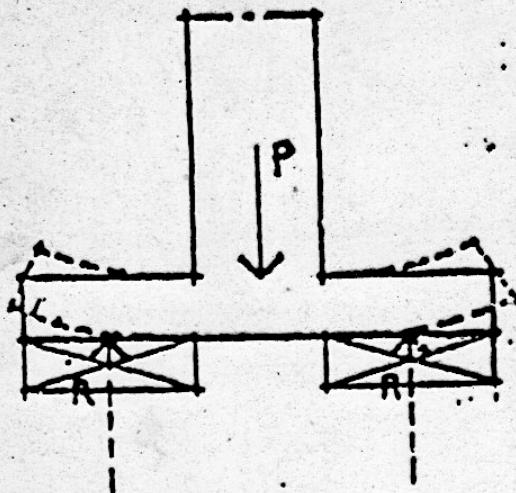
1. the width of foundation (b)
2. the foundation depth (z)



n- value for vertical stress distribution

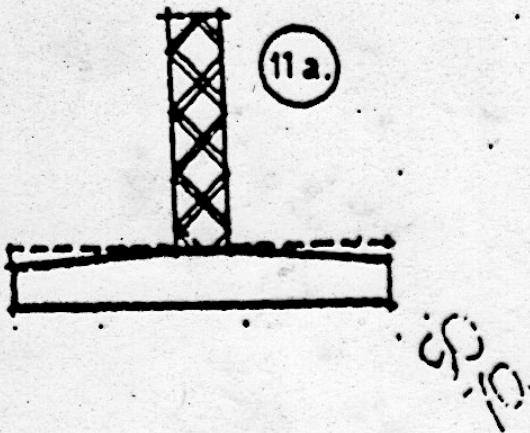
Permitted vertical stress increase (σ) in kN/m^2	100	200	300	400	500
B 5 ($5,0 \text{ N/mm}^2$)	1.6	2.0	2.0	not permitted	
B 10 ($10,0 \text{ N/mm}^2$)	1.1	1.6	2.0	2.0	2.0
B 15 ($15,0 \text{ N/mm}^2$)	1.0	1.3	1.6	1.8	2.0
B 25 ($25,0 \text{ N/mm}^2$)	1.0	1.0	1.2	1.4	1.6
B 35 ($35,0 \text{ N/mm}^2$)	1.0	1.0	1.0	1.2	1.3

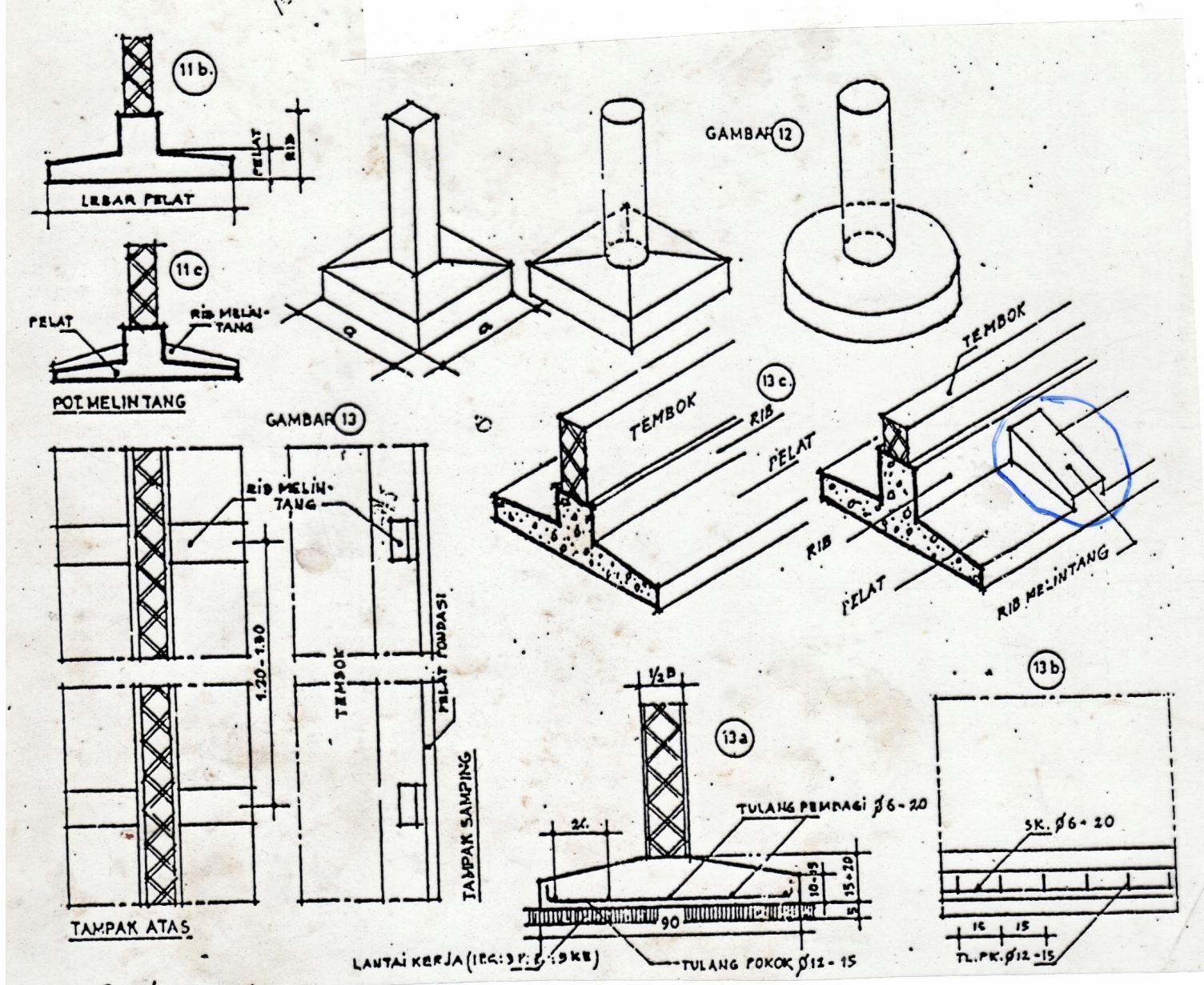
GAMBAR 11.



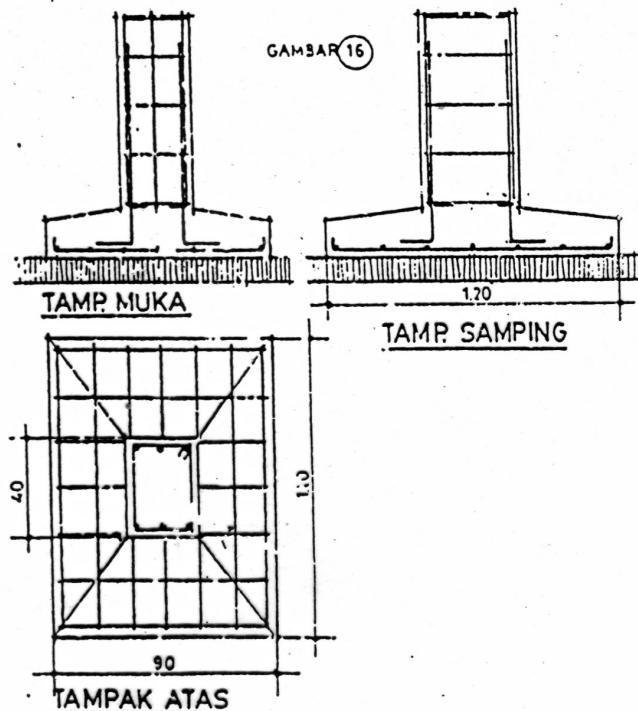
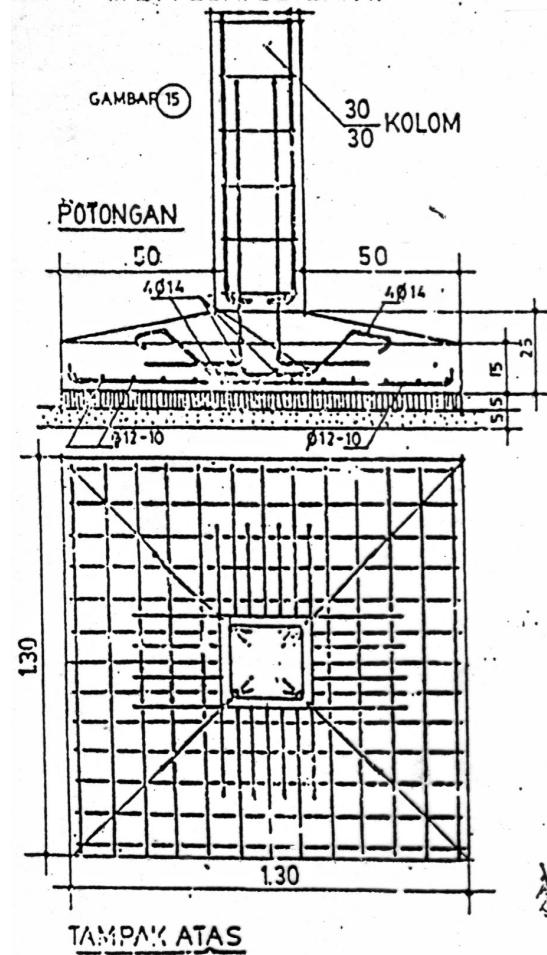
Skema pembebaan pada
pondasi pelat beton

11 a.

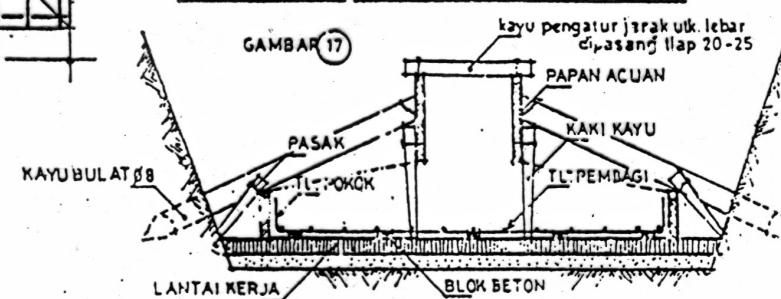




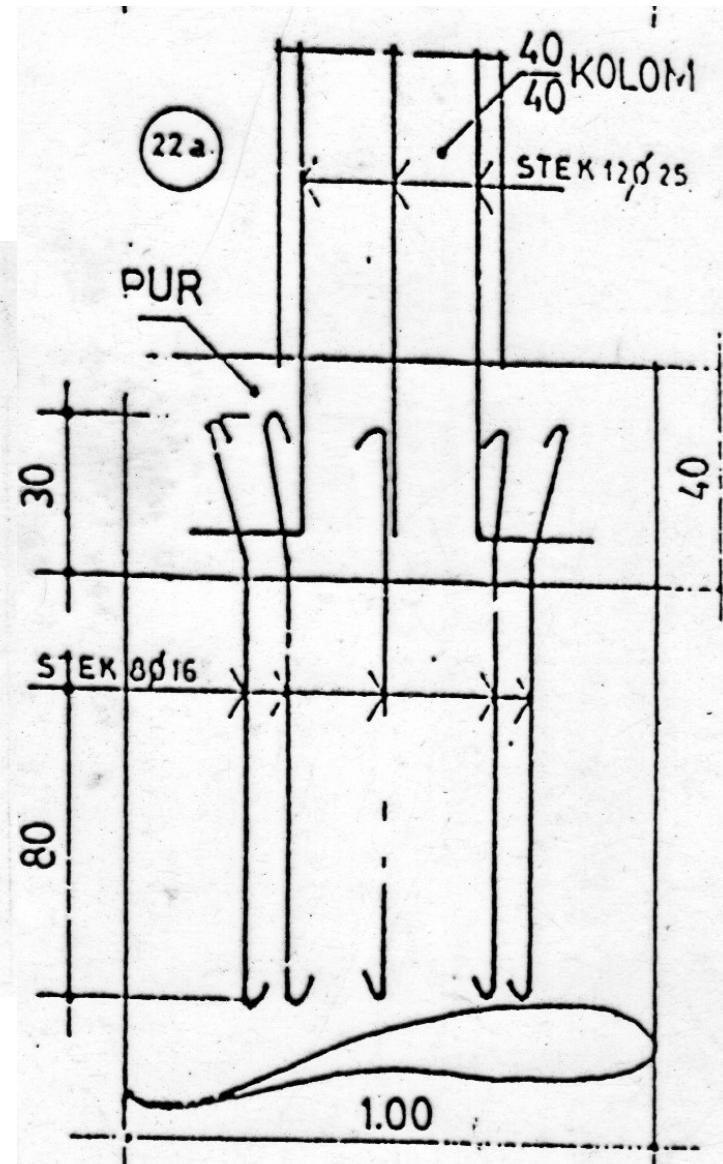
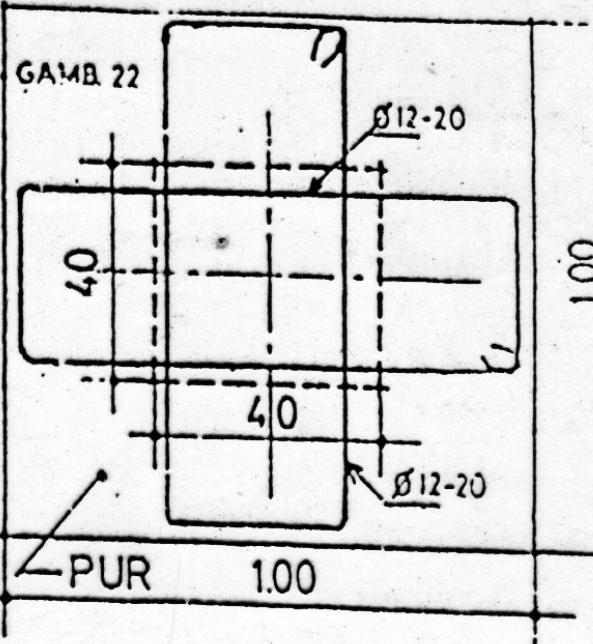
DETAIL PERTEMUAN KOLOM DG. PONDASI PELAT SETEMPAT

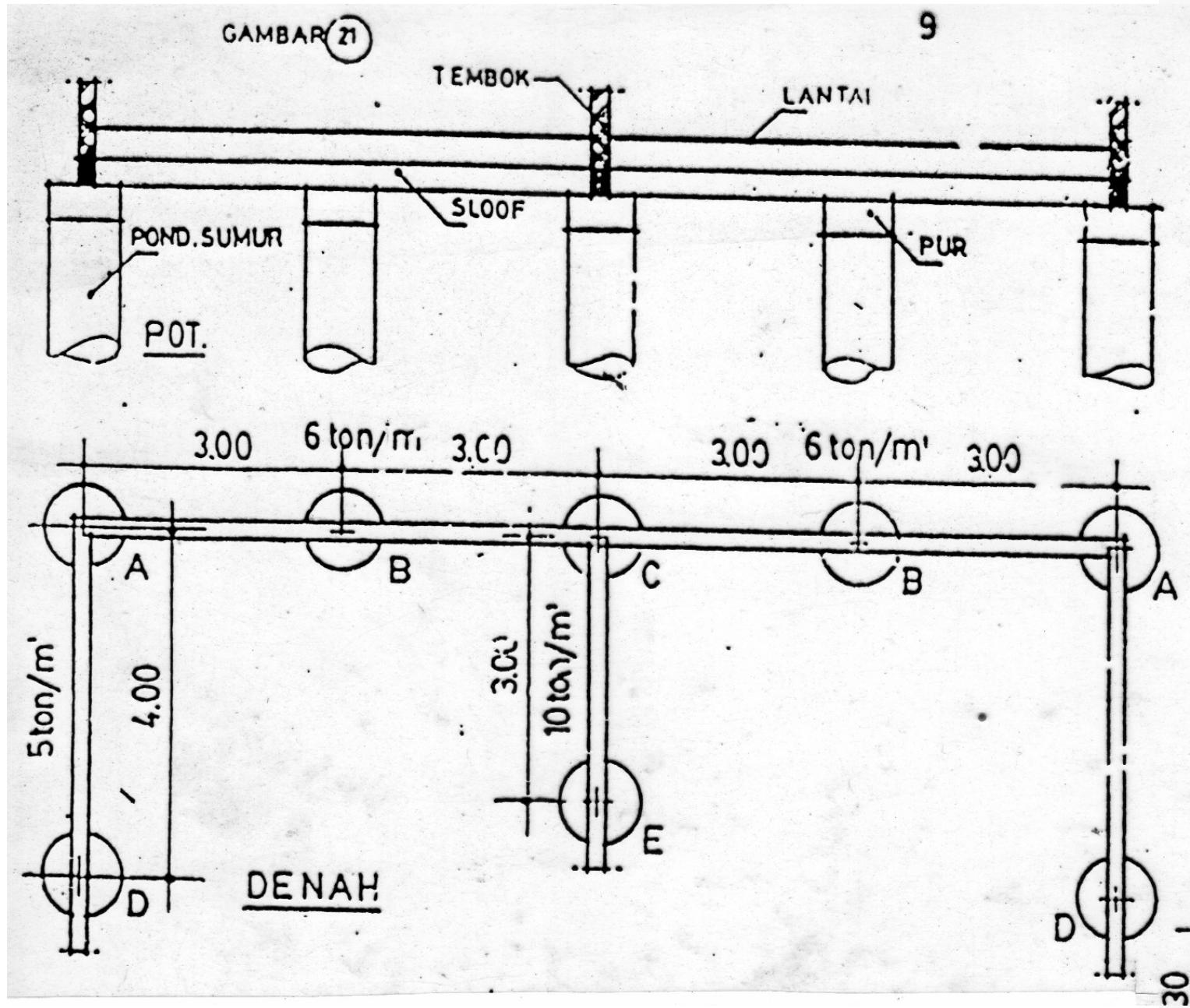


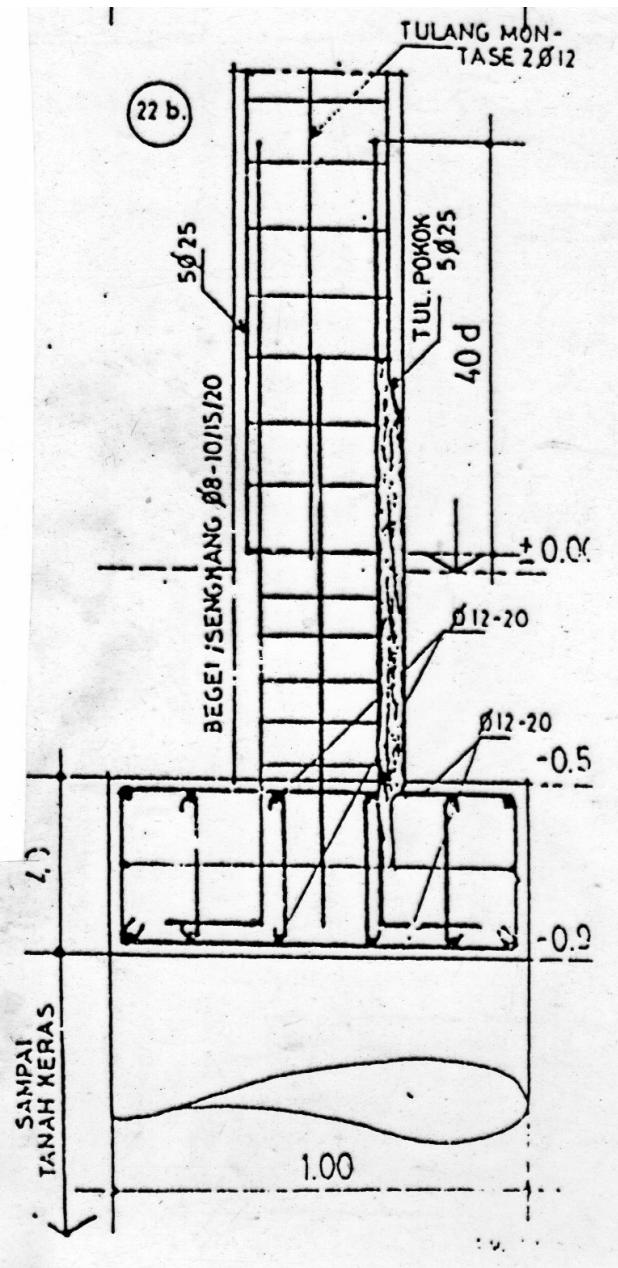
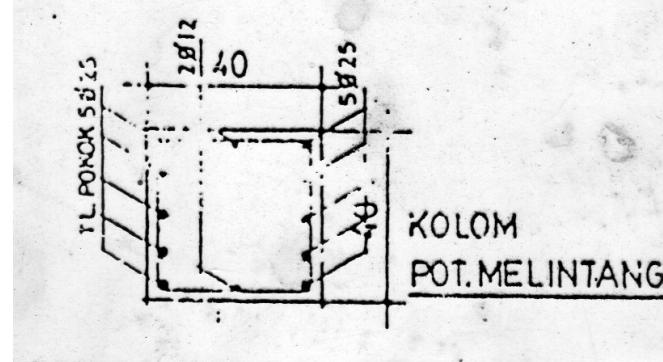
CARA PEMBUATAN PONDASI PELAT BETON

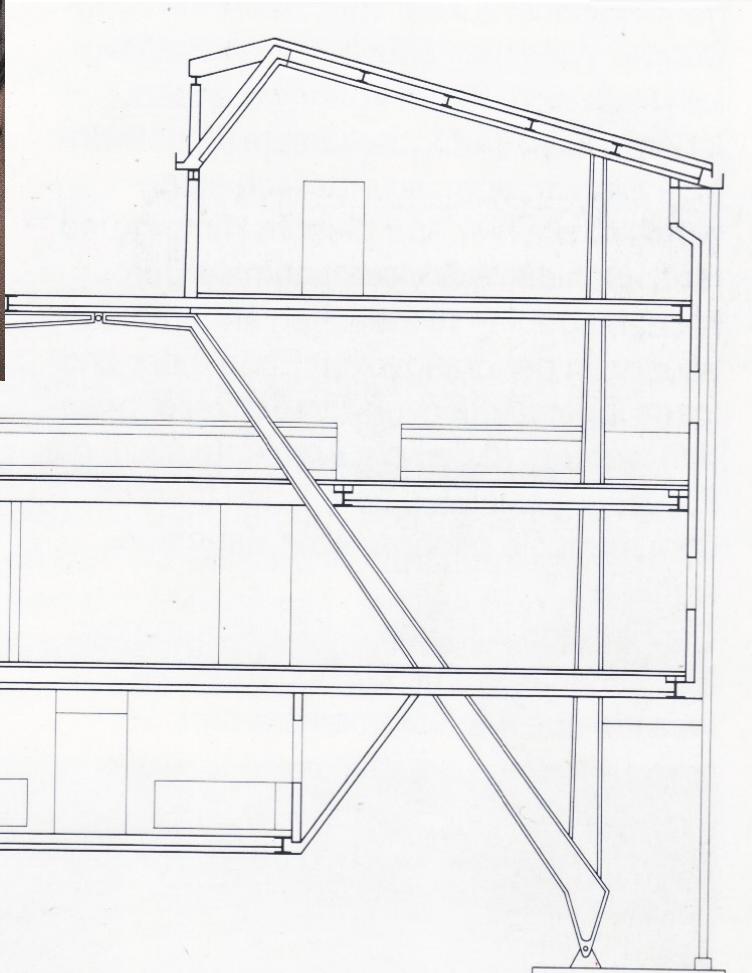


CETAIL PONDASI SUMUI





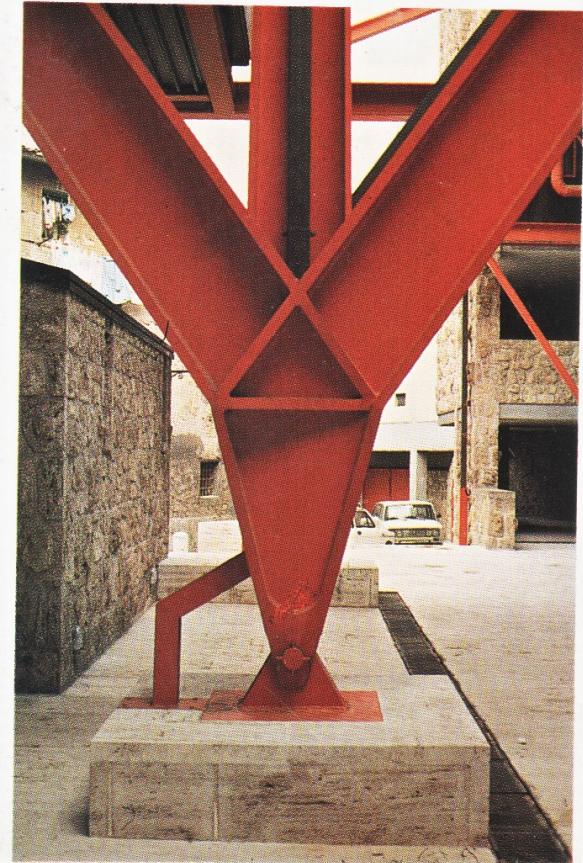
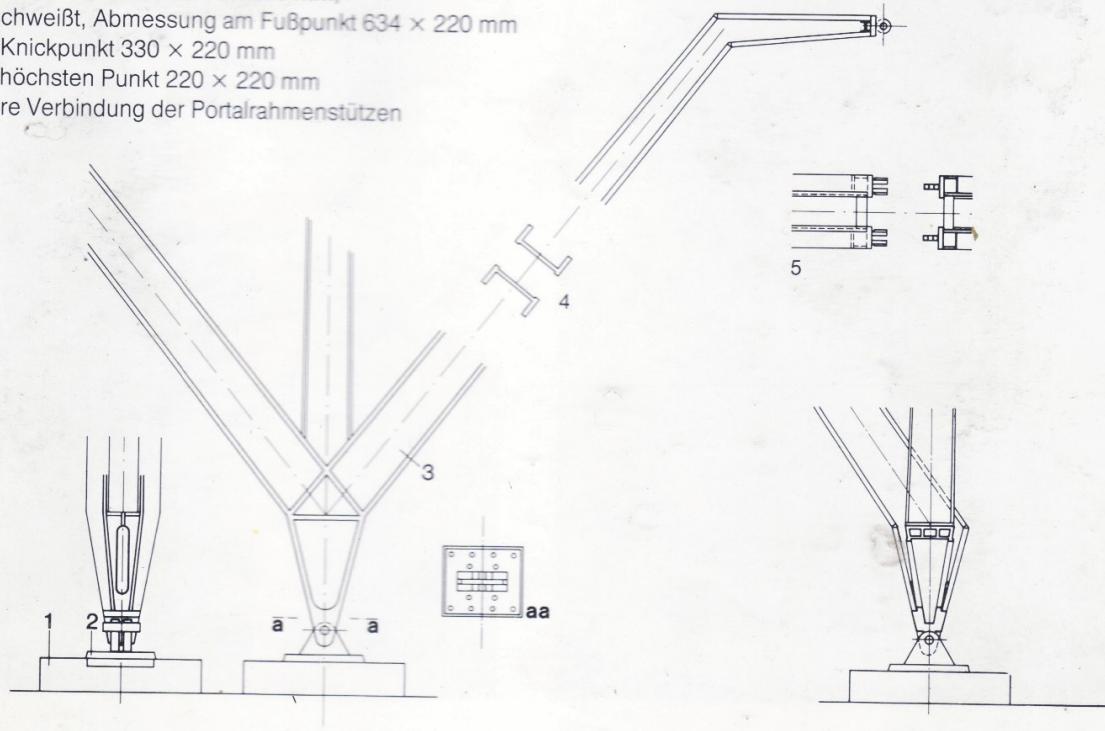




KREATIFITAS GEOMETRI BANGUNAN – HUBUNGAN RANGKA DAN PONDASI

Stützenfuß Maßstab 1:100

- 1 Travertin Stützenfuß 1600/1600/340 mm
- 2 Stahlplatte am Stützenfuß 800/700/70 mm
- 3 Portalrahmen
- 4 2 LJ-Profile im Abstand von 300 mm,
geschweißt, Abmessung am Fußpunkt 634 x 220 mm
am Knickpunkt 330 x 220 mm
am höchsten Punkt 220 x 220 mm
- 5 obere Verbindung der Portalrahmenstützen



KREATIFITAS GEOMETRI BANGUNAN – HUBUNGAN RANGKA DAN PONDASI

Rumah tinggal keluarga Ir. Daryanto

Jalan Srinindito Selatan IV/16, Samarang Barat 50148 70/54 cm
Rencana : Drs. Heinz Fried, Archit. SIA, Jl. Pemuda Barat M/2

Potongan A-A 1:20, Terali jendela 1:20
Dm. 1:50
1 meter.

